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Barotropic instabilities of the Agulhas Current system and their relation to ring formation

by Henk A. Dijkstra$^1$ and Wilhelmus P. M. De Ruijter$^1$

ABSTRACT

Recent work has shown that different steady retroflection regimes, a viscous and an inertial regime, exist for the Agulhas Current system in an idealized geometry. In this paper, instabilities of the barotropic steady flows are considered by solving the linear stability problem numerically. Barotropic instabilities occur as so-called Hopf bifurcations in the viscous regime, with corresponding patterns related to Rossby basin modes. Depending on the value of the reduced gravity parameter, these instabilities may introduce intermonthly to interannual variability into the retroflection region. Finite amplitude development of these instabilities display ‘ring-like’ localized anomaly patterns which travel around the tip of the continent. The results demonstrate that, within the barotropic context, (i) the frequency of the ring formation is set by the physics of the large-scale instabilities and (ii) the rectification processes due to these instabilities decrease the degree of retroflection of the mean state. The latter result suggests that the dominant mechanism of the retroflection is captured within the steady balances.

1. Introduction

Roughly once every two months, a large ring is shed from the Agulhas Current and propagates westward into the South Atlantic (Gordon and Haxby, 1990; Feron et al., 1992; Schouten et al., 2000). The Agulhas Current itself turns eastward in an impressive retroflection, leaving the rings as main processes of interbasin exchange. As the rings transport heat and salt from the Indian to the Atlantic Ocean, they are potentially important for the global thermohaline circulation (Gordon, 1985). Estimates on the amount of mass, heat and salt involved in the exchange differ widely, both from observations and from different ocean general circulation models (De Ruijter et al., 1999).

In a detailed numerical model study (Chassignet and Boudra, 1988), ring formation is considered in an isopycnic (and in most cases two-layer) model for an idealized domain under a wide range of conditions. In the relatively viscous regime (the low Rossby number case E1), 4 rings per year are found on average. The frequency of ring cut-off was shown to be related to the interaction of the top-layer flow dynamics and ocean basin-mode patterns propagating in the bottom layer. Energy transformations in the flow were monitored but
did not give any conclusive evidence whether a type of instability plays a primary role in the ring formation and shedding process. In the more inertial regime (the large Rossby number case E10), the frequency decreases to 4 rings in 10 years. In this case, a strong coupling exists between the ring shedding and the retroflecting and meandering mean current. During a ring shedding event, the bottom layer kinetic energy triples in magnitude and a mixed barotropic-baroclinic instability was suggested to be involved. Processes setting the frequency of the ring shedding events were in this case difficult to identify.

A pure inertial mechanism of ring formation has been proposed recently in the context of a reduced gravity model (Nof and Pichevin, 1996; Pichevin et al., 1999). When a current retroflects, a momentum imbalance exists under a rather restricting set of conditions. Development of rings can solve this so-called “retroflection paradox” and the theory developed provides estimates of spatial scales of the rings and their propagation speed. Numerical results show reasonable agreement with the theoretically provided bounds on length scale and mass flux of the rings. Only the period of ring shedding appears slightly more sensitive to parameter changes and varies within a range of 80–160 days. The existence of these different views of ring formation is intriguing and their connection is not easily established; model formulations and corresponding dynamics are very different.

A recent study (Dijkstra and De Ruijter, 2001), we reconsidered the small basin configuration (De Ruijter and Boudra, 1985; Chassignet and Boudra, 1988) and analyzed the steady states within a barotropic shallow water model as a function of the lateral friction coefficient (horizontal Ekman number $E$). With modern tools of numerical bifurcation theory, unstable steady states could also be determined and two regimes of steady retroflection were shown to exist: a viscous and an inertial one. In the viscous regime, retroflection occurs through viscous choking; the viscous boundary layer is thick enough to allow the current to bridge the gap from the southern tip of the continent to the latitude of zero wind stress curl. In the inertial regime, inertial effects are strong enough to bridge this gap (De Ruijter and Boudra, 1985). The most important result in Dijkstra and De Ruijter (2001) is that retroflection characteristics are already present in the steady balances and that rectification processes due to barotropic/baroclinic instabilities are not essential for retroflection to occur.

In this paper, we consider the stability of these steady solutions by solving the linear stability problem numerically within an (equivalent) barotropic shallow water model. The different unstable modes are identified and their characteristics are studied as the Rossby deformation radius is varied. For the barotropic case, transient flows in the unstable regime are computed and the physics of the dominant time scale of variability and the changes in the time mean state are investigated.

2. Model and methods

The model used (Dijkstra and De Ruijter, 2001) is an (equivalent) barotropic shallow water model in spherical coordinates, modeling the zonal velocity $u$, meridional velocity $v$, and sea-surface height anomaly $h$ (with respect to some equilibrium depth $H$) of the
wind-driven flow in the upper layer having density \( \rho \). Below this layer is a motionless layer with density \( \Delta \rho + \rho \). This leads to the reduced gravity \( g' = g \Delta \rho / \rho \). In this paper, we will use only the idealized basin geometry as in De Ruijter and Boudra (1985). The domain chosen is \( \phi_W = 10E, \phi_E = 32E, \theta_S = 42S \) and \( \theta_N = 30S \), and the basin has a flat bottom. The zonal size of the domain varies with latitude (from about 2100 km at the northern boundary to about 1800 km at the southern boundary) and has a meridional extent of 1300 km. A ‘rectangular’ continent is present over the domain \( \phi_W = 19.5E, \phi_E = 20.5E, \theta_S = 35S \) and \( \theta_N = 30S \).

The wind stress forcing is prescribed as an analytical profile of the form
\[
\tau^\phi(\theta) = \cos(6.37(\theta - \theta_\star)) ; \tau^\theta = 0
\]
and \( \tau^\phi(\theta) \) is plotted in Figure 1 for \( \theta_\star = -39.5 \). The amplitude \( \tau_0 \) was chosen to be \( \tau_0 = 0.2 \) Pa. In this way, the maximum westerly wind stress is located at \( \theta = -39.5 \); i.e., about 400 km south of the tip of the continent. Although the wind stress curl is not exactly zero at this location (because of the spherical coordinates), the deviation is small because of the small basin size.

With \( r_0 \) denoting the radius of the earth, the governing shallow water equations are nondimensionalized using scales \( r_0, H \), a characteristic horizontal velocity \( U \), \( r_0/U \) and \( \tau_0 \) for length, layer depth, velocity, time and wind stress, respectively. These become
Table 1. Standard values of parameters in the (equivalent) barotropic model for the idealized small basin. The value of $A_H$ (and consequently $E$) is the reference value and $E$ will be used here as control parameter.

**Dimensional parameters**

<table>
<thead>
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<th>Parameter</th>
<th>Value</th>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>$r_0$</td>
<td>$6.4 \times 10^6$ m</td>
<td>$\tau_0$</td>
<td>$2.0 \times 10^{-1}$ Pa</td>
</tr>
<tr>
<td>$H$</td>
<td>$1.0 \times 10^3$ m</td>
<td>$A_H$</td>
<td>$3.3 \times 10^2$ m$^2$s$^{-1}$</td>
</tr>
<tr>
<td>$g'$</td>
<td>$0.1$ m s$^{-2}$</td>
<td>$U$</td>
<td>$1.0 \times 10^{-1}$ m s$^{-1}$</td>
</tr>
<tr>
<td>$\rho_0$</td>
<td>$1.0 \times 10^1$ kg m$^{-3}$</td>
<td>$\Omega$</td>
<td>$7.5 \times 10^{-5}$ s$^{-1}$</td>
</tr>
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**Dimensionless parameters**

<table>
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<tr>
<th>Parameter</th>
<th>Value</th>
<th>Parameter</th>
<th>Value</th>
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<tbody>
<tr>
<td>$\alpha$</td>
<td>$1.3 \times 10^{-2}$</td>
<td>$E$</td>
<td>$5.0 \times 10^{-8}$</td>
</tr>
<tr>
<td>$\epsilon$</td>
<td>$1.0 \times 10^{-4}$</td>
<td>$F$</td>
<td>$1.0 \times 10^4$</td>
</tr>
</tbody>
</table>

\[
\epsilon \left( \frac{\partial u}{\partial t} + \frac{u}{\cos \theta} \frac{\partial u}{\partial \phi} + v \frac{\partial u}{\partial \theta} - uv \tan \theta \right) - v \sin \theta
= - \epsilon F \frac{\partial h}{\cos \theta \partial \phi} + E \left( \nabla^2 u - \frac{u}{\cos^2 \theta} - \frac{2 \sin \theta \partial v}{\cos^2 \theta \partial \phi} \right) + \alpha \frac{\tau^\phi}{h} \tag{2a}
\]

\[
\epsilon \left( \frac{\partial v}{\partial t} + \frac{u}{\cos \theta} \frac{\partial v}{\partial \phi} + v \frac{\partial v}{\partial \theta} + u^2 \tan \theta \right) + u \sin \theta
= - \epsilon F \frac{\partial h}{\partial \theta} + E \left( \nabla^2 v - \frac{v}{\cos^2 \theta} + \frac{2 \sin \theta \partial u}{\cos^2 \theta \partial \phi} \right) + \alpha \frac{\tau^\theta}{h} \tag{2b}
\]

\[
\frac{\partial h}{\partial t} + \frac{1}{\cos \theta} \left( \frac{\partial (hu)}{\partial \phi} + \frac{\partial (hv \cos \theta)}{\partial \theta} \right) = 0. \tag{2c}
\]

In the dimensionless equations, the following parameters appear: the Rossby number $\epsilon$, the Froude number $F$, the Ekman number $E$, and the wind stress coefficient $\alpha$. Expressions for these parameters are

\[
\epsilon = \frac{U}{2\Omega r_0}; \quad F = \frac{g' H}{U^2}; \quad E = \frac{A_H}{2\Omega r_0}; \quad \alpha = \frac{\tau_0}{2\Omega \rho H U} \tag{3}
\]

where $\Omega$ is the angular velocity of the earth. Standard values of both dimensional and nondimensional parameters are given in Table 1 and are similar as in Dijkstra and De Ruijter (2001). The only difference is the value of $F$, which in the barotropic limit is equal to $10^6$, the value in the limit $g' \to g$.

Branches of the steady states are followed in parameter space, mainly in the control parameter $E$, using continuation techniques. For each solution, the retroreflection index $\mathcal{R}_t$, as defined in Dijkstra and De Ruijter (2001), is plotted. This retroreflection index is the ratio of the maximum westward volume transport ($\Phi_w(20)$) at the tip of the continent ($20E$) and...
the maximum southward volume transport \( \Phi_s(-35) \) at 35S. In the results below, \( R \) is computed as

\[
R = 1 - \frac{\Phi_w(20)}{\Phi_s(-35)}. \tag{4}
\]

If there is no westward transport \( \Phi_w(20) = 0 \), then there is complete retro/fection and \( R = 1 \). On the other hand, if all the incoming southward flow from the Agulhas Current is transported westward, then there is no retro/fection at all and \( R = 0 \). The results in Dijkstra and De Ruijter (2001) indicate that for solutions computed on 1/4° (as is the resolution for most results in De Ruijter and Boudra (1985)), the Ekman number should be larger than \( E = 2 \times 10^{-7} \).

We use methods of numerical bifurcation theory to determine steady solutions of the shallow water model and to determine their stability (Dijkstra, 2000). Eqs. (2) can be written in operator form as

\[
\mathcal{M} \frac{\partial \mathbf{u}}{\partial t} + \mathcal{L} \mathbf{u} + \mathcal{N}(\mathbf{u}) = \mathbf{F} \tag{5}
\]

where \( \mathcal{L}, \mathcal{M} \) are linear operators, \( \mathcal{N} \) is a nonlinear operator, \( \mathbf{u} \) is the vector of dependent quantities and \( \mathbf{F} \) contains the forcing of the system and appropriate boundary conditions are taken into account. To determine the steady states \( \tilde{\mathbf{u}} \) of the system of equations when parameters are changed, the problem

\[
\mathcal{L} \tilde{\mathbf{u}} + \mathcal{N}(\tilde{\mathbf{u}}) = \mathbf{F} \tag{6}
\]

has to be solved. This set of partial differential equations is discretized by a central volume finite difference method on an 88 \( \times \) 48 grid, providing horizontal resolution of 1/4°, and a system of nonlinear algebraic equations of the form

\[
\mathbf{G}(\mathbf{x}, \mu) = 0 \tag{7}
\]

emerges. Here \( \mathbf{x} \) is a vector with dimensions \( d = 3 \times 88 \times 48 = 12,672 \), consisting of the unknowns at the gridpoints and \( \mu \) is the control parameter, for example \( \mu = E \). To determine branches of steady solutions of (7) as \( \mu \) is varied, the pseudo-arclength method is used (Keller, 1977; Seydel, 1994). The branches \( (\mathbf{x}(s), \mu(s)) \) are parametrized by an ‘arclength’ parameter \( s \) and an additional equation is obtained by an approximation of the normalization condition of the tangent, i.e.

\[
\dot{x}_0^T(x - x_0) + \dot{\mu}_0(\mu - \mu_0) - \Delta s = 0 \tag{8}
\]

where \( (x_0, \mu_0) \) is a known starting solution or a previously computed point on a particular branch, \( \Delta s \) is the steplength and the dot indicates differentiation to \( s \). To follow steady solutions along branches in parameter space, an Euler-Newton scheme is used (Seydel, 1994).

To determine the linear stability of a steady state, perturbations \( \tilde{\mathbf{u}} \) are considered. With
u = \tilde{u} + \hat{u}, linearizing (5) around \tilde{u} and separating \hat{u} = \hat{u}e^{\sigma t} gives an eigenvalue problem of the form

\[(\mathcal{L} + \mathcal{N}_u)\hat{u} = -\sigma \mathcal{M}\hat{u} \quad (9)\]

where \mathcal{N}_u is the derivative of the operator \mathcal{N} with respect to u. Discretization of this eigenvalue problem leads to a generalized algebraic eigenvalue problem of the form

\[\mathcal{A}\hat{\mathbf{x}} = \sigma \mathcal{B}\hat{\mathbf{x}} \quad (10)\]

where \mathcal{A} is a nonsingular, nonsymmetric \(d \times d\) matrix and \(\sigma = \sigma_r + i\sigma_i\) is the eigenvalue. The problem (10) is solved by the Jacobi-Davidson QZ-method (JDQZ). With this method, one can compute several eigenvalues and optionally eigenvectors near a specified target. Details of the method are described in Sleijpen and Van der Vorst (1996) and the implementation of JDQZ in an earlier version of our continuation code in Van Dorsselaer (1997).

3. Results: Stability bounds

In this section, first the linear stability of the barotropic steady states computed in Dijkstra and De Ruijter (2001) is discussed and subsequently, effects of changes in the Rossby deformation radius are studied.

As mentioned above, the barotropic (flat bottom) case can be obtained in the limit \(g' \to g\) giving the value \(F = 10^6\). Two bifurcation diagrams are shown in Figure 2 for two values of the layer thickness \(H\). The curves are similar to Figure 5 in Dijkstra and De Ruijter (2001), except that now the stability of the steady flows is indicated. A solid (dotted) curve indicates a stable (unstable) flow, while the stability boundaries are marked by the solid triangles. Here, the steady states becomes unstable to oscillatory instabilities; such a transition is called a Hopf bifurcation (Seydel, 1994). For \(H = 1000\) m, this stability boundary is located at \(E_c = 2.6 \times 10^{-7}\) whereas for \(H = 250\) m, it is found at \(E_c = 8.2 \times 10^{-7}\). As could be expected, the case with higher inertially controlled flow is more unstable, because of the larger horizontal shear.

At the Hopf bifurcation on the curve for \(H = 1000\) m in Figure 2, the steady state flow pattern, shown as a contour plot of the layer thickness anomaly \(h\), is plotted in Figure 3a. A strong Agulhas Current is present near the eastern side of the continent but it has almost no retroflexion. The pattern of the oscillatory mode which destabilizes the steady state can be determined from the solution of the linear stability problem (10) with eigenvalue \(\sigma\). The corresponding complex eigenfunction \(\hat{x} = \hat{x}_R + i\hat{x}_I\) provides the time periodic disturbance structure \(P(t)\) with angular frequency \(\sigma_i\) and growth rate \(\sigma_r\) to which the steady state becomes unstable, i.e.

\[P(t) = e^{\sigma t}[\hat{x}_R \cos (\sigma t) - \hat{x}_I \sin (\sigma t)]. \quad (11)\]
Propagation features of a neutral mode \( (\sigma_r = 0.0) \) can be determined by first looking at \( P(\pi/(2\sigma_i)) = \hat{x}_i \) and then at \( P(0) = \hat{x}_R \). The dimensional period \( \mathcal{P} \) of the oscillation is given by \( \mathcal{P} = 2r_0\pi/(U\sigma_i) \).

The patterns of the real and imaginary part of the layer thickness anomalies of the eigenvector, destabilizing the steady state in Figure 3a, are shown in Figure 3b–c. The dimensionless angular frequency of the mode \( (\sigma_i = 1.12 \times 10^2) \) corresponds to a dimensional period \( \mathcal{P} = 1.35 \) months. The perturbation patterns are basin wide and have strong similarities to inviscid Rossby basin modes (Pedlosky, 1987), which can be labeled \((n, m)\) and differ with respect to the number of zeroes of the streamfunction in zonal and meridional direction. The patterns here would be ‘guessed’ as the \((2, 1)\) mode which in the inviscid case has an oscillation period of about a month (Chassignet and Boudra, 1988; Dijkstra and Katsman, 1997). Hence, the pattern in Figure 3b–c can be identified as a destabilized Rossby basin mode. In this case, the presence of the continent deforms the basin mode as it propagates westward.

The steady flow with smaller layer thickness \((H = 250 \text{ m})\) destabilizes at larger values of the lateral friction. The steady state (Fig. 4a) at criticality \( (E_c = 8.2 \times 10^{-7}) \) shows more of a tendency to retroreflect, although from Figure 2, it can be seen that steady retroreflection becomes pronounced only at smaller values of \( E \). The patterns of the layer

![Figure 2](image-url)
Figure 3. (a) Steady state at the Hopf bifurcation ($E_c = 2.6 \times 10^{-7}$) on the curve for $H = 1000$ m in Figure 2, shown as a contour plot of the layer thickness anomaly $h$. (b) Real part of the eigenvector ($\hat{x}_R$) at the Hopf bifurcation associated with $P(t)$ as in (11). (c) Imaginary part of the eigenvector ($\hat{x}_I$) at the Hopf bifurcation associated with $P(t)$ as in (11). These patterns can be identified as a destabilized Rossby basin mode. In this case, the presence of the continent deforms the basin mode as it propagates westward.
Figure 4. (a) Steady state at the Hopf bifurcation ($E_c = 8.2 \times 10^{-7}$) for $H = 250$ m in Figure 2, shown as a contour plot of the layer thickness anomaly $h$. (b) Real part of the eigenvector ($\hat{x}_R$) at the Hopf bifurcation associated with $P(t)$ as in (11). (c) Imaginary part of the eigenvector ($\hat{x}_I$) at the Hopf bifurcation associated with $P(t)$ as in (11). Together, $\hat{x}_R$ and $\hat{x}_I$ provide a picture of the propagating mode, according to (11).
thickness anomalies of the most unstable mode at Hopf bifurcation (Fig. 4b–c) resemble again a westward propagating Rossby basin mode (‘guessed’ as the pattern coming from the inviscid (4, 1) Rossby basin mode) and its oscillating period is about 1.4 months ($\sigma_i = 1.09 \times 10^2$). The main difference between this mode and the mode in Figure 3 (in the case $H = 1000$ m) is that the pattern is more localized within the high shear region of the steady state and has a smaller zonal scale.

For the case $H = 1000$ m, the values of the lateral Ekman number $E$ at which the Hopf bifurcation occurs (and the corresponding angular frequency of oscillation at criticality) are plotted in Figure 5 for several values of $F$. The frequency of oscillation (dashed curve) is increasing monotonically with $g^\prime$ as is expected from elementary Rossby wave theory. For $F = 1000$, the value of $\sigma_i$ has decreased to $\sigma_i = 7.8$ which corresponds to an oscillation period of about 1.6 years. The critical value $E_c$ has no monotonic behavior and there seems to be an optimal value of instability (around $F = 5 \times 10^4$) and stability (around $F = 10^4$). The steady state at $F = 10^4$ (Fig. 6a), plotted at criticality ($E_c = 1.2 \times 10^{-7}$), shows more recirculation in the return flow compared to that in Figure 3a. This is due to the much smaller Ekman number of the flow which makes it more inertially controlled. Although the pattern of the mode destabilizing this steady state derives (Fig. 6b–c) again from a westward propagating Rossby basin mode, its spatial scale has decreased substantially. It would be ‘guessed’ now to derive from the (5, 2) inviscid basin.

Figure 5. Dependence of the critical Ekman number, $E_c$, (drawn) at which the steady state becomes unstable to an oscillatory mode and the angular frequency ($\sigma_i$) at criticality (dashed) on the Froude number $F$. The markers correspond to the actually computed points, which are connected by straight lines.
Figure 6. (a) Steady state at the Hopf bifurcation for $F = 10^4$, $E_c = 1.2 \times 10^{-7}$ and $H = 1000$ m. (b) Real part of the eigenvector ($\hat{x}_R$) at the Hopf bifurcation associated with $P(t)$ as in (11). (c) Imaginary part of the eigenvector ($\hat{x}_I$) at the Hopf bifurcation associated with $P(t)$ as in (11).
mode. Note that the critical Ekman number considered in the latter case is in the regime where numerical resolution was considered just sufficient to resolve steady states (Dijkstra and De Ruijter, 2001); these critical values may shift slightly when higher resolution is used.

4. Results: Transient supercritical flows

To investigate how the instabilities turn the steady states into transient flows as critical conditions are exceeded (i.e., values of $E$ smaller than those at the Hopf bifurcation), several transient flow computations are performed. The issues which are addressed in this section are the rectification of the mean flow due to the instabilities and the dominant frequency of variability in the nonlinear regime. Starting condition for all computations is an unstable steady state at the particular supercritical values of $E$ chosen. Only the barotropic case is considered ($F = 10^6$).

For $E = 2.0 \times 10^{-7}$ and $H = 1000$ m, the deviation from the perturbed steady state and the approach to the limit cycle can be seen in the retrofection index and, in equilibrium, regular periodic behavior results (Fig. 7). The period of the finite amplitude oscillation is slightly larger than one month and hence corresponds well to that of the eigenmode at the Hopf bifurcation in Figure 2. When the flow patterns over one period of oscillation are considered and the difference of the instantaneous state and the unstable steady state (at $E = 2.0 \times 10^{-7}$) is plotted, one actually sees the anomalies propagating as is suggested by the unstable mode at criticality (Fig. 3b–c). The time-averaged flow over exactly one oscillation period is shown in Figure 7b together with the unstable steady state (Fig. 7c) at the same value of $E$. The differences between the flows are due to nonlinear rectification processes. The latter are small in this case, because the system is still not far above criticality ($E$ near $E_c$). The retrofection index of the time mean state is $\mathcal{R}_m = -0.094$, whereas the steady state value is $\mathcal{R}_s = -0.014$ (Fig. 2). Hence, this indicates that the rectification due to barotropic instabilities decreases the degree of retrofection.

For the more inertially controlled case of $H = 250$ m, the retrofection index varies so strongly that, at times, there is complete retrofection ($\mathcal{R} = 1$). The oscillations are irregular (Fig. 8) which indicates that several modes are involved in the dynamical behavior of the flow. Although the integration period is only two years, it is clear that the dominant frequency of the variability remains intermonthly, indicating that the first mode which is destabilized is still controlling the dynamics. The time mean state over the last year of the simulation for $E = 2 \times 10^{-7}$ is shown in Figure 8b, with the unstable steady state for the same value of $E$ shown in Figure 8c. As can be seen, the steady state is substantially rectified, but the time-mean state still shares the same retrofection properties. The retrofection index of the time mean state is $\mathcal{R}_m = 0.236$, whereas that of the steady state is $\mathcal{R}_s = 0.336$ (Fig. 2). Again, this indicates that the strongly time-dependent features of the flow due to barotropic instabilities decrease the degree of retrofection.
Figure 7. (a) Time series of the retroreflection index for the barotropic case with $H = 1000$ m, $E = 2.0 \times 10^{-7}$. Starting point is the unstable steady state which is slightly perturbed into the direction of the mode destabilizing at the Hopf bifurcation. (b) Time mean state averaged over exactly one oscillation period in Figure 7a. (c) The unstable steady state calculated at the same value of the Ekman number ($H = 1000$ m, $E = 2 \times 10^{-7}$).
Figure 8. (a) Time series of the retrofection index for the barotropic case with $H = 250$ m, $E = 2.0 \times 10^{-7}$. (b) Time mean state computed over one year (over the interval as indicated by the dash-dotted line in Fig. 8a). (c) The unstable steady state at the same value of the Ekman number.
5. Summary and discussion

In this paper, the stability of the steady flow states computed in a barotropic and reduced gravity shallow water model of the Agulhas Current system (Dijkstra and De Ruijter, 2001) was considered. All steady states destabilize at some critical value of the lateral friction (i.e., horizontal Ekman number $E_c$), which depends on the layer depth and the value of the reduced gravity. In each case, the first mode which is destabilized has a pattern which is strongly related to a Rossby basin mode. Its period is not very dependent on the layer depth $H$ (and thus on inertia), but strongly dependent on the value of the reduced gravity and varies from intermonthly in the barotropic case to interannual for the standard value of $g'$ (i.e., $F = 10^4$ in Fig. 5).

For $E$ slightly smaller than $E_c$, periodic behavior appears. The destabilized basin modes are the origin of the variability on the steady state which consists of ‘ring-like’ localized patterns propagating westward around the continent. The frequency is determined by that of the first mode which destabilizes at criticality. Under slightly supercritical conditions, the time-mean state of the time-dependent flow is different than the unstable steady state, at the same values of the parameters, through rectification processes. The retroreflection of this time-mean state is, for the cases considered, smaller than that for the unstable steady state. This shows that, although retroreflection is a time-mean feature, it depends on the nonlinear interaction of time-dependent processes. Due to the presence of the westward propagating disturbances, apparently the time-mean retroreflection loop moves farther westward. The fact that these time-dependent processes here decrease the degree of retroreflection is an important result since it suggests that the actual retroreflection in the time-mean state is inherited from the steady balances. If it would have been otherwise (more retroreflection due to rectification processes), then the relevance of the steady states would probably become questionable. Whether baroclinic instabilities and their rectification promote retroreflection needs further study.

For smaller values of $H$, the instabilities occur already on steady states with a weak retroreflection. The transient flow is, therefore, more complicated at strongly supercritical conditions, due to the destabilization of more modes (with respect to situations at larger $H$). However, the dominant period of the barotropic transient flow still appears to be in the intermonthly range and the time-mean state again shows a lower degree of retroreflection than the steady state. The results here indicate that the origin of the frequency of ‘ring formation’ may be set by the physics of the large-scale barotropic instabilities. They certainly provide a deeper level of understanding of the numerical results in Chassignet and Boudra (1988). One can now conclude that, in their case $E1$, the period of ring shedding indeed derives from a barotropic instability of a Rossby basin mode. This is fully consistent with the time scale found and the patterns of anomalies in the lower layer. In their upper layer, the Rossby basin mode signal is not so clear, likely because of strong interactions of the unstable mode with the upper layer flow. The barotropic instability mechanism here cannot explain the decrease in frequency in the inertial regime. Indeed, as Chassignet and Boudra (1988) mention, baroclinic processes are likely important for this to occur.
When the Rossby deformation radius is decreased (smaller $F$), or the wind stress increased at constant $F$, at some point the upper layer thickness will become zero somewhere in the domain. This limit may be interesting since it probably forms the connection between results in Chassignet and Boudra (1988) and those in Pichevin et al. (1999). In Pichevin et al. (1999), the background flow structure is prescribed, through inflow/outflow conditions, without considering its origin in the wind and/or buoyancy forcing. For a near-inertial flow in this configuration, retroreflection is guaranteed to occur (Ou and De Ruijter, 1986) even with slip conditions at the continental boundaries. However, the coupling of the mean retroreflecting current to the large-scale wind forcing, and consequently to the far field flow, is important. Hence, the central question is whether these types of background flows can be generated by a reasonable forcing.

Retroreflection, and consequently ring formation, exists only under no-slip conditions in the set-up of Chassignet and Boudra (1988) as their model configuration does not allow upper interface outcrop. All flows are forced under a given wind stress, but one can argue that these flows are still too viscous to realize a near-inertial current. Moreover, the effect of the lateral boundaries (in particular the closed western boundary) may be too strong. Hence, here the question is whether a steady momentum imbalance is approached within a more global domain in the limit of very small lateral friction. If one can set up the forcing of the wind and the basin geometry such that a type of retroreflecting flow appears as in Pichevin et al. (1999), then the occurrence of a saddle node bifurcation would be the signature of the ‘retroreflection paradox’ in the language of dynamical systems; work on this connection is currently in progress.

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